

Fundamental Equation

$$\frac{dN_A}{dt} = F_{A0} - F_A + \int^V r_A dV$$

Design Equations

	Conversion Basis	Molar Basis
Batch	$N_{A0} \frac{dX}{dt} = -r_A V \quad t_1 = N_{A0} \int_0^X \frac{dX}{-r_A V}$	$\frac{dN_A}{dt} = r_A V \quad t_1 = \int_{N_{A1}}^{N_{A0}} \frac{dN_A}{-r_A V}$
CSTR	$V = \frac{F_{A0}(X_{out} - X_{in})}{-r_{Aout}}$	$V = \frac{F_{Ain} - F_{Aout}}{-r_{Aout}}$
PFR	$F_{A0} \frac{dX}{dV} = -r_A \quad V_1 = F_{A0} \int_{X_{in}}^{X_{out}} \frac{dX}{-r_A}$	$\frac{dF_A}{dV} = r_A \quad V_1 = \int_{F_{A1}}^{F_{A0}} \frac{dF_A}{-r_A}$
PBR	$F_{A0} \frac{dX}{dW} = -r'_A \quad W_1 = F_{A0} \int_{X_{in}}^{X_{out}} \frac{dX}{-r'_A}$	$\frac{dF_A}{dW} = r'_A \quad W_1 = \int_{F_{A1}}^{F_{A0}} \frac{dF_A}{-r'_A}$

Ideal gas law:

$$pV = nRT$$

$$R = 8.314 \frac{J}{mol.K} = 1.987 \frac{cal}{mol.K}$$

Arrhenius Equation:

$$k_A(T) = A \cdot \exp\left[\frac{E_A}{-RT}\right] \quad k_A(T) = k_A(T_0) \cdot \exp\left[\frac{E_A}{R}\left(\frac{1}{T_0} - \frac{1}{T}\right)\right]$$

$$K_C(T) = K_C(T_0) \cdot \exp\left[\frac{\Delta H_{rxn}^0}{R}\left(\frac{1}{T_0} - \frac{1}{T}\right)\right]$$

Stoichiometry:

For Reaction: $aA + bB \rightarrow cC + dD$ Liquid Phase: $C_i = C_{A0}(\Theta_i - v_i X)$

$$\text{Gas Phase: } C_i = \frac{C_{A0}(\Theta_i + v_i X)}{1 + \varepsilon X} \left(\frac{P}{P_0}\right) \left(\frac{T_0}{T}\right) \quad v = v_0(1 + \varepsilon X) \left(\frac{T}{T_0}\right) \left(\frac{P_0}{P}\right)$$

$$\Theta_i = \frac{F_{i0}}{F_{A0}} = \frac{C_{i0}}{C_{A0}} = \frac{y_{i0}}{y_{A0}} \quad \delta = \frac{d}{a} + \frac{c}{a} - \frac{b}{a} - 1 \quad \varepsilon = y_{A0} \delta$$

Packed Beds:

laminar turbulent

$$\frac{dP}{dz} = -\frac{G}{\rho g_c D_p} \left(\frac{1-\phi}{\phi^3}\right) \left[\frac{150(1-\phi)\mu}{D_p} + 1.75G\right] \quad \frac{dP}{dW} = -\frac{\alpha}{2} \frac{P_0}{P/P_0} \left(\frac{T}{T_0}\right) (1 + y_{A0} \delta X)$$

$$\beta_0 = -\frac{G}{\rho_0 g_c D_p} \left(\frac{1-\phi}{\phi^3}\right) \left[\frac{150(1-\phi)\mu}{D_p} + 1.75G\right] \quad \alpha = \frac{2\beta_0}{A_c \rho_c (1-\phi) P_0} \quad dW = (1-\phi) A_c \rho_c dz$$

If isothermal and $\delta = 0$ or X is very small:

$$\frac{P}{P_0} = (1 - \alpha W)^{1/2}$$

Energy Balance

$$\frac{d\hat{E}_{sys}}{dt} = \dot{Q} - \dot{W}_s + \sum F_i H_i|_{in} - \sum F_i H_i|_{out}$$

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For Steady State System in Single Phase	Adiabatic System (CSTR, PFR, PBR, Batch)
$0 = \dot{Q} - \dot{W}_s - F_{A0} \sum_{i=1}^n \Theta_i \bar{C}_{P_i} (T - T_{i0}) - \Delta H_{Rx}(T) F_{A0} X$ where $H_{Rx}(T) = \Delta H_{Rx}^o(T_R) + \underbrace{\Delta C_p}_{\sum \nu_i C_{P_i}} (T - T_R)$	Conversion $X = \frac{\sum \Theta_i C_{P_i} (T - T_0)}{-[\Delta H_{Rx}^o(T_R) + \Delta C_p (T - T_R)]}$ Temperature $T = \frac{X[-\Delta H_{Rx}^o(T_R)] + \sum \Theta_i C_{P_i} T_0 + X \Delta C_p T_R}{\sum \Theta_i C_{P_i} + X \Delta C_p}$

PFR with heat exchange

$$\frac{dT}{dV} = \frac{\overbrace{r_A \Delta H_{Rx}}^{Q_g \text{ "Generated"}} - \overbrace{Ua(T - T_a)}^{Q_r \text{ "Removed"}}}{\sum F_i C_{P_i}}$$

Unsteady State CSTR and Semibatch

$$\frac{dT}{dt} = \frac{\dot{Q} - \dot{W}_s - \sum F_{i0} \bar{C}_{P_i} (T - T_0) + (-\Delta H_{Rx})(-r_A V)}{\sum N_i C_{P_i}}$$

Multiple Reactions:

Selectivity and Yield

Instantaneous Selectivity	$S_{D/U} = r_D / r_U$
Overall Selectivity	$\tilde{S}_{D/U} = F_D / F_U$
Instantaneous Yield	$Y_{D/A} = r_D / -r_A$
Overall Yield	$\tilde{Y}_{D/U} = F_D / (F_{A0} - F_A)$

External and Internal Diffusion:

$$W_{AZ} = k_c (C_{AB} - C_{AS})$$

System with reaction only on external surface area: $C_{AS} = \frac{k_c}{k'' + k_c} C_{AB}$

$$Re = \frac{\rho U d_p}{\mu} \quad Sh = \frac{k_c d_p}{D_{AB}} \quad Sc = \frac{\nu}{D_{AB}}$$

Correlation for flow around a sphere: $Sh = 2 + 0.6 Re^{1/2} Sc^{1/3}$

$$\eta = \frac{r_{obs}}{r_{max}} = \frac{\tanh(\phi_1)}{\phi_1}, \phi_1 = L_P \sqrt{\frac{k}{D_{AB}^e}} \text{ where } D_{AB}^e = \frac{D_{AB} \phi_p \sigma_c}{\tilde{\tau}}$$

and $L_P = x_P \text{ (slab)}, \frac{R_P}{3} \text{ (sphere)}, \frac{R_P}{2} \text{ (cylinder)}$

Enzyme Kinetics:

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Michaelis – Menten Equation: $r_{product} = \frac{V_{max}[S]}{K_M + [S]}$

Lineweaver-Burke Analysis: $\frac{1}{r_p}$ versus $\frac{1}{[S]}$

Integrals:

$$\int_0^X x^a dx = \frac{x^{a+1}}{a+1}, \quad a \neq -1$$

$$\int_0^X \frac{dX}{1 + \varepsilon X} = \frac{1}{\varepsilon} \ln(1 + \varepsilon X)$$

$$\int_0^X x^{-1} dx = \ln(x)$$

$$\int_0^X \frac{1 + \varepsilon X}{1 - X} dX = (1 + \varepsilon) \ln\left(\frac{1}{1 - X}\right) - \varepsilon X$$

$$\int_0^X \frac{dX}{1 - X} = \ln\left(\frac{1}{1 - X}\right)$$

$$\int_0^X \frac{1 + \varepsilon X}{(1 - X)^2} dX = \frac{(1 + \varepsilon)X}{1 - X} - \varepsilon \ln\left(\frac{1}{1 - X}\right)$$

$$\int_0^X \frac{dX}{(1 - X)^2} = \frac{X}{1 - X}$$

$$\int_0^W (1 - \alpha W)^{1/2} dW = \frac{2}{3\alpha} [1 - (1 - \alpha W)^{3/2}]$$

$$\int_0^X \frac{(1 + \varepsilon X)^2}{(1 - X)^2} dX = 2\varepsilon(1 + \varepsilon) \ln(1 - X) + \varepsilon^2 X + \frac{(1 + \varepsilon)^2 X}{1 - X}$$

$$\int_0^X \frac{dX}{(1 - X)(\Theta_B - X)} = \frac{1}{\Theta_B - 1} \ln\left(\frac{\Theta_B - X}{\Theta_B(1 - X)}\right), \quad \Theta_B \neq 1$$

$$\frac{dy}{dt} + P(t)y = Q(t), \quad I(t) = e^{\int P(t)}, \quad \frac{d(yI(t))}{dt} = Q(t)I(t), \quad y = \frac{1}{I(t)} \int Q(t)I(t)dt$$

Roots for: $ax^2 + bx + c$ $\frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$